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Research Article

Adaptive Fuzzy Synchronization of Fractional-Order Chaotic (Hyperchaotic) Systems with Input Saturation and Unknown Parameters

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We investigate the synchronization problem of fractional-order chaotic systems with input saturation and unknown external disturbance by means of adaptive fuzzy control. An adaptive controller, accompanied with fractional adaptation law, is established, fuzzy logic systems are used to approximate the unknown nonlinear functions, and the fractional Lyapunov stability theorem is used to analyze the stability. This control method can realize the synchronization of two fractional-order chaotic or hyperchaotic systems and the synchronization error tends to zero asymptotically. Finally, we show the effectiveness of the proposed method by two simulation examples.

1. Introduction

Recent studies showed that a large number of physical phenomena of nature and chemical processes, such as viscosity systems, colored noise, electrolyte electrode polarization, electromagnetic waves, and many actual systems can be described by fractional-order differential equations, making the slowly developed fractional calculus be a resurgence of interest [1-10]. Today, fractional-order systems described by fractional operators play a very important role in control fields [11-13]. Using the traditional integer-order differential equations as a method of describing dynamic system models has great limitation in biological engineering, cell engineering, neural network engineering, and some other emerging fields. However, the models established by fractional calculus can often achieve more satisfying and unexpected results [9, 14, 15]. Actually, the physical models established by the theory of fractional-order calculus are more concise and accurate in presentation when describing the complex problems of physics. In addition, the fractional controller not only can expand the freedom of the controlled system but also is able to

obtain better control performance. Furthermore, the feature that fractional calculus has the function of memory makes the system's states in the future be related to the previous and current states. Thus the memory and genetic characteristics of certain processes and materials can be expressed more accurately, which is conducive to improving the control effect of the systems [16, 17].

It is well known that chaos has potential application values and great prospect in secure communication and other areas [18–22]. Recently, fractional-order chaotic systems and hyperchaotic systems have been studied in a widespread way and have been payed close attention with the deepening of theoretical research of fractional-order systems [23–26]. Many scholars have studied the synchronization control problems for fractional-order chaotic systems. So far, there are many control methods for fractional-order nonlinear chaotic systems (such as drive-response method, finite-time synchronization, nonlinear feedback method, adaptive synchronization control method, nonlinear disturbance observer method, nonlinear coupling method, sliding method, PC method, Lyapunov function activated method,

and synchronization control method [27–33]). It is worth noting that the above literatures which study the problem of fractional-order chaotic systems synchronization have a basic assumption that the controller does not have any restrictions. However, almost all actuators in actual control systems have full amplitude or amplitude constraint problem (the amplitude of the output of the controller is limited artificially for reliability [34]). In addition, the presence of the input saturation of the control systems tends to attenuate the good performance of the system and even leads to instability of the closed-loop system. So many scholars have conducted extensive research in integer-order systems with input saturation in the recent years (literatures [35–37], etc.). Little work has been done to study the synchronous control of fractional-order nonlinear chaotic systems with input saturation.

In this paper, the adaptive fuzzy synchronization of uncertain fractional-order nonlinear systems with input saturation and external disturbance is investigated on the basis of the above discussions. Fuzzy logic systems are used to approximate the fully unknown nonlinear functions of the systems. A fractional adaptive fuzzy synchronization controller is designed, and we prove the stability of the chaotic systems according to the fractional Lyapunov stability criterion. The main work of this paper can be concluded as follows: (1) The synchronization of fractional-order chaotic systems with input saturation and external disturbance is discussed in this paper. (2) An adaptive fuzzy synchronization controller is designed and fractional adaptive laws are designed to update the values of the parameters online.

2. Preliminaries

2.1. Preliminaries of Fractional Calculus. With the history of more than 300 years, there are many definitions of fractional calculus. But the most commonly used definitions are Grünwald-Letnikov, Caputo, and Riemann-Liouville definitions [11]. We choose Caputo's derivative in this paper as its Laplace transform requires the initial values of the classical integer-order systems.

The α th fractional integral operator is defined as

$$\mathcal{J}_{\tau}^{-\alpha} f(\tau) =_{0} D_{\tau}^{-\alpha} f(\tau) = \frac{1}{\Gamma(\alpha)} \int_{0}^{\tau} (\tau - \nu)^{\alpha - 1} f(\nu) d\nu, \quad (1)$$

where $\Gamma(z) = \int_0^\infty \tau^{z-1} e^{-\tau} d\tau$ represents Euler's Gamma function. The α th fractional derivative operator is given as

$$D_t^{\alpha} f(\tau) = \frac{1}{\Gamma(n-\alpha)} \int_0^{\tau} (\tau - \nu)^{n-\alpha-1} f^{(n)}(\nu) d\nu, \qquad (2)$$

where $n - 1 \le \alpha < n$ and n is an integer. And the Laplace transform of the formed formula (2) is

$$\int_0^\infty e^{-st} D_\tau^\alpha f(\tau) d\tau = s^\alpha F(s) - \sum_{k=0}^{n-1} s^{\alpha-k-1} f^{(k)}(0).$$
 (3)

The following properties of fractional calculus hold.

Property 1 (see [38]). Suppose that $x(\tau) \in C^1[0,T], T > 0$; then

$$D_{\tau}^{\alpha_1} D_{\tau}^{\alpha_2} x(\tau) = D_{\tau}^{\alpha_1 + \alpha_2} x(\tau), \qquad (4)$$

where $\alpha_1, \alpha_2 > 0$ and $\alpha_1 + \alpha_2 \leq 1$.

Property 2 (see [38]). The linearity of the Caputo fractional operator is as follows:

$$D_{\tau}^{\alpha} \left(\lambda x \left(\tau \right) + \omega y \left(\tau \right) \right) = \lambda D_{\tau}^{\alpha} x \left(\tau \right) + \omega D_{\tau}^{\alpha} y \left(\tau \right), \tag{5}$$

where λ and ω are two real constants.

Remark 1. If *c* is a constant, then its Caputo derivative is 0. Namely, $D_{\tau}^{\alpha}c = 0$. Particularly, we have $D_{\tau}^{\alpha}0 = 0$.

Property 3 (see [11]). Let $x(\tau) \in C^1[0,T]$ and $0 < \alpha < 1$; then

$$D_{\tau}^{-\alpha}D_{\tau}^{\alpha}x(\tau) = x(\tau) - x(0),$$

$$D_{\tau}^{\alpha}D_{\tau}^{-\alpha}x(\tau) = x(\tau).$$
(6)

Note that the above properties hold if and only if $0 < \alpha < 1$. Consequently, only the case where $0 < \alpha < 1$ is involved in the controller design and stability analysis. For convenience, in the rest of this paper, we always assume that $\alpha \in (0, 1)$.

2.2. Fuzzy Logic Systems. A fuzzy logic system (FLS) consists of four parts (cf. [8, 9, 39–44]): the knowledge base, the fuzzifier, the fuzzy inference engine working on the fuzzy rules, and the defuzzifier. Usually, a fuzzy logic system is modeled by

$$\widehat{y} = \frac{\sum_{j \in J} w_j(t) \,\mu_j(x(t))}{\sum_{j \in J} \mu_j(x(t))},\tag{7}$$

where \widehat{y} (a Lipschitz continuous mapping from a compact subset $\Omega\subseteq \mathcal{R}^n$ to the real line \mathcal{R}) is called the output of the fuzzy logic system, $x=[x_1,\ldots,x_n]^T\in C^1[\mathcal{F},\Omega]$ (the set of all continuous mappings from $\mathcal{F}=[0,+\infty)\subseteq \mathcal{R}$ to Ω which have continuous derivatives) is called the input vector which is defined by $x(t)=[x_1(t),\ldots,x_n(t)]^T~(\forall t\in \mathcal{F}),$ $J=\prod_{i=1}^n\mathcal{F}_i,\,\mathcal{F}_i$ consists of N_i fuzzy sets $(1\leq i\leq n),\,\mu_j$ (a mapping from \mathcal{R}^n to the closed unit interval $[0,1]\subseteq \mathcal{R}$) is called the membership function of rule $j~(j\in J)$, and w_j (a mapping from \mathcal{F} to \mathcal{R}) is called the centroid of the jth consequent set $(j\in J)$; we may identify J with $\{1,2,\ldots,N\}$ for the sake of convenience. Write $\mathcal{W}(t)=[w_1(t),\ldots,w_N(t)]^T$ and $\varphi(x(t))=[q_1(x(t)),q_2(x(t)),\ldots,q_N(x(t))]^T$, where q_j (called the jth fuzzy basis function, $j\in J$) is a continuous mapping (and thus $\varphi\Omega\to\mathcal{R}^N$ is continuous) defined by

$$q_{j}\left(x\left(t\right)\right) = \frac{w_{j}\left(t\right)}{\sum_{s \in J} \mu_{s}\left(x\left(t\right)\right)}.$$
 (8)

Then system (7) can be rewritten as

$$y = \mathcal{W}^T \varphi(X). \tag{9}$$

In contrast to conventional control techniques, fuzzy logic systems are best utilized in complex ill-defined processes that can be controlled by a skilled human operator without much knowledge of their underlying dynamics. The basic idea behind fuzzy logic systems is to incorporate the "expert experience" of a human operator in the design of the controller in controlling a process whose input-output relationship is described by a collection of fuzzy control rules involving linguistic variables rather than a complicated dynamic model.

The fuzzy logic system (9) is employed to approximate the unknown nonlinear function $f(\mu)$ in this paper. It can be expressed as

$$f(\mu) = \mathcal{W}^{*T} \varphi(\mu) + \epsilon(\mu), \tag{10}$$

where $\epsilon(\mu)$ is the ideal vector of the approximation error. \mathcal{W}^* is the ideal weight matrix which can be expressed as

$$\mathcal{W}^* = \arg\min_{\mathcal{W}} \left[\sup \left| \hat{f}(\mu) - f(\mu) \right| \right], \tag{11}$$

where $\hat{f}(\mu)$ is the estimation of $f(\mu)$.

3. Adaptive Fuzzy Synchronization Controller **Design and Stability Analysis**

3.1. Problem Statement. Consider the following fractionalorder chaotic systems:

$$D_t^{\alpha} x(t) = Ax(t) + f(x(t)), \qquad (12)$$

$$D_t^{\alpha} y(t) = Cy(t) + g(y(t)) + \text{sat}(u) + d(t),$$
 (13)

where $x(t) = [x_1(t), \dots, x_n(t)]^T \in \mathbb{R}^n$ is the state vector of the drive system (12) and $y(t) = [y_1(t), \dots, y_n(t)]^T \in \mathbb{R}^n$ is the state vector of the response system (13). $f_i(\cdot)$ and $g_i(\cdot)$, i = 1, 2, ..., n, are two unknown nonlinear functions, A and $C \in \mathbb{R}^{n \times n}$ are two constant matrices, $d(t) \in \mathbb{R}^n$ is the external disturbance, $sat(u) \in \mathbb{R}^n$ represents the input saturation, and $u(t) \in \mathbb{R}^n$ is the control input.

Remark 2. In theoretical analysis, one often hopes that the input value and the output value can keep proportionally synchronized change when the former is relatively small. However, when the input value increases to a certain extent due to the system limitation factor, the output value of the actual conditions is no longer increasing but tends to or stays at a certain value in practical systems. This is said to be "saturation" phenomenon which is shown in Figure 1.

Definition 3 (see [45, 46]). A mapping from R^n to R^n sat : $\nu \to \operatorname{sat}(\nu)$ is called a saturator, where $\nu = [\nu_1, \nu_2, \dots, \nu_n]^T \in$ R^n and $sat(v) = [sat(v_1), sat(v_2), ..., sat(v_n)]^T$. The definition of sat(u) is as follows:

$$sat (u(t)) = \begin{cases}
 u_r, & u(t) \ge u_r \\
 u(t), & u_l < u(t) < u_r \\
 u_l, & u(t) \le u_l.
\end{cases}$$
Then (17) can be rewritten as
$$D_t^{\alpha} e(t) = Ce(t) + (C - A)x(t) + g(y(t)) - f(x(t)) + u(t) + \delta(t) + d(t).$$

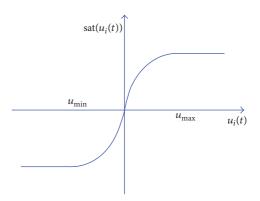


FIGURE 1: The phenomenon of saturation.

Suppose that the part that exceeds the saturation limiter is referred to as $\delta(t)$; then one has

$$\delta(t) = \begin{cases} u_r - u(t), & u(t) \ge u_r \\ 0, & u_l < u(t) < u_r \end{cases}$$

$$u_l - u(t), & u(t) \le u_l,$$
(15)

where u_r and u_l are called saturated amplitude satisfying u_l < 0 and $u_r > 0$.

Assumption 4. The external disturbance $d_i(\cdot)$ is a bounded continuous function. Namely, there exists an unknown constant $\rho_i > 0$ such that

$$|d_i(\cdot)| \leq \rho_i, \quad (i=1,2,\ldots,n).$$
 (16)

Remark 5. It should be pointed out that Assumption 4 is reasonable. We just need the boundaries of the external disturbances, and their exact values are not needed in the process of designing the controller.

The objective of our work is to design an appropriate adaptive fuzzy controller such that the synchronization error e(t) = y(t) - x(t) tends to zero asymptotically (namely, $\lim_{t\to\infty}\|e(t)\|=0).$

3.2. Controller Design. The dynamical equation of the synchronization error can be described as

$$D_{t}^{\alpha}e(t) = Ce(t) + (C - A)x(t) + g(y(t)) - f(x(t)) + sat(u) + d(t).$$
(17)

Based on the definition of sat(u), we can obtain that

$$sat(u) = u(t) + \delta(t). \tag{18}$$

Then (17) can be rewritten as

$$D_{t}^{\alpha}e(t) = Ce(t) + (C - A)x(t) + g(y(t)) - f(x(t)) + u(t) + \delta(t) + d(t).$$
(19)

Consider

$$h(x(t), y(t)) = h(t)$$

$$= (C - A)x(t) + g(y(t)) - f(x(t))$$
(20)
$$+ \delta(t).$$

Nothing that the nonlinear function h(t) is unknown, it can be approximated, through the fuzzy logic system (9), as

$$\widehat{h}_{i}(t) = \mathcal{W}_{i}^{T}(t)\,\varphi_{i}(x)\,,\tag{21}$$

where $\mathcal{W}_i^* = \arg\min_{\mathcal{W}_i(t)} [\sup |h_i(t) - \widehat{h}_i(t, \mathcal{W}_i(t))|]$. Let the unknown constant estimation error of the fuzzy logic systems and the approximation error, respectively, be

$$\widetilde{W}_{i}(t) = W_{i}(t) - W_{i}^{*},$$

$$\epsilon_{i}(t) = h_{i}(t) - \hat{h}_{i}(t, W_{i}^{*}).$$
(22)

The following assumption is needed in the controller design.

Assumption 6. Suppose that the estimation error $\epsilon_i(t)$ is bounded; namely, $|\epsilon_i| \leq \epsilon_i^*$, where $\epsilon_i^* > 0$ is an unknown constant (i = 1, 2, ..., n).

Then the estimated error of unknown nonlinear function h(t) can be written as

$$\widehat{h}(t, \mathcal{W}) - h(t) = \widehat{h}(t, \mathcal{W}) - \widehat{h}(t, \mathcal{W}^*) + \widehat{h}(t, \mathcal{W}^*)$$

$$- h(t)$$

$$= \widehat{h}(t, \mathcal{W}) - \widehat{h}(t, \mathcal{W}^*) - \epsilon(t)$$

$$= \widetilde{\mathcal{W}}^T(t) \varphi(x) - \epsilon(t),$$
(23)

where $W^* = [W_1^*, W_2^*, ..., W_m^*]^T$.

Based on the above discussion, the synchronization controller u(t) can be designed as

$$u(t) = -Ke(t) - \mathcal{W}^{T}(t) \varphi(x) - H \operatorname{sign}(e(t))$$
$$-\widehat{\rho} \operatorname{sign}(e(t)),$$
(24)

where $K = \operatorname{diag}[k_1, k_2, \ldots, k_n] \in \mathbb{R}^{n \times n}$ and $k_i > 0$ is the designed parameter. $H = \operatorname{diag}[\epsilon_1^*, \ldots, \epsilon_n^*]$, $\widehat{\rho} = \operatorname{diag}[\widehat{\rho}_1, \widehat{\rho}_2, \ldots, \widehat{\rho}_n] \in \mathbb{R}^{n \times n}$, and $\widehat{\rho}_i$ is the estimation of ρ_i ($i = 1, 2, \ldots, n$). The fuzzy parameters and $\widehat{\rho}_i(t)$ are, respectively, updated by

$$D_t^{\alpha} \mathcal{W}_i(t) = \mu_i e_i(t) \, \varphi_i(x) \,, \tag{25}$$

$$D_t^{\alpha} \widehat{\rho}_i(t) = \gamma_i \left| e_i(t) \right|, \tag{26}$$

where μ_i , $\gamma_i > 0$ are positive design parameters.

Remark 7. The above fractional adaptive laws are used to update the adjustable parameters. Notice that (26) can also be written as the following equation:

$$\widehat{\rho}_{i}(\nu) = \widehat{\rho}_{i}(0) + \frac{1}{\Gamma(\alpha)} \int_{0}^{\nu} \gamma_{i}(\nu - \tau)^{\alpha - 1} \left| e_{i}(\tau) \right| d\tau. \tag{27}$$

Definition 8 (see [11]). Mittag-Leffler functions (M-L functions) with one parameter and two parameters are, respectively, defined as

$$E_{\alpha}(t) = \sum_{k=0}^{\infty} \frac{t^k}{\Gamma(\alpha k + 1)},$$
(28)

$$E_{\alpha,\beta}(t) = \sum_{k=0}^{\infty} \frac{t^k}{\Gamma(\alpha k + \beta)},$$
(29)

where α , β > 0. The Laplace transform of (29) is expressed as

$$\mathscr{L}\left(t^{\beta-1}E_{\alpha,\beta}\left(-\lambda t^{\alpha}\right)\right) = \frac{s^{\alpha-\beta}}{s^{\alpha}+\lambda}, \quad \left(\operatorname{Re}\left(s\right) > |\lambda|^{1/\alpha}\right), \quad (30)$$

where $t \ge 0$ and $\lambda \in R$.

Lemma 9 (fractional Lyapunov second method [11]). *Let the origin be the equilibrium point of the following system:*

$$D_t^{\alpha} x(t) = f(t, x(t)), \tag{31}$$

where $x(t) \in \mathbb{R}^n$ is the system variable and $f(t,x(t)) \in \mathbb{R}^n$ is nonlinear function that satisfies the local Lipschitz condition. If there exists Lyapunov function $\mathcal{V}(t,x(t))$ and positive parameters h_1 , h_2 , and h_3 such that

$$h_{1} \|x\left(t\right)\| \leq \mathcal{V}\left(t, x\left(t\right)\right) \leq h_{2} \|x\left(t\right)\|,$$

$$D_{t}^{\alpha} \mathcal{V}\left(t, x\left(t\right)\right) \leq -h_{3} \|x\left(t\right)\|,$$
(32)

then system (31) is asymptotically stable.

Lemma 10 (see [47]). Suppose that $x(t) \in \mathbb{R}^n$ is a continuously differentiable function; then one has

$$\frac{1}{2}D_t^{\alpha}x^T(t)x(t) \le x^T(t)D_t^{\alpha}x(t). \tag{33}$$

Lemma 11 (fractional monotonic principle [47]). If $D_t^{\alpha} x(t) \ge 0$, then x(t) is monotonically increasing in $[0, +\infty)$. If $D_t^{\alpha} x(t) \le 0$, then x(t) is monotonically decreasing in $[0, +\infty]$.

Lemma 12 (see [9, 47]). Let $V_1(t) = (1/2)x^2(t) + (1/2)y^2(t)$; x(t) and $y(t) \in R$ are two continuous functions. If there exists a positive constant k satisfying

$$D_t^{\alpha} V_1(t) \leqslant -kx^2(t), \tag{34}$$

then one has the following inequality:

$$x^{2}(t) \leq 2V_{1}(0) E_{\alpha}(-2kt^{\alpha}).$$
 (35)

Lemma 13. Suppose that $V(t) = (1/2)x^{T}(t)x(t) + (1/2)y^{T}(t)y(t)$, where $x(t), y(t) \in \mathbb{R}^{n}$ have continuous derivative. If there exists a constant h > 0 such that

$$D_{+}^{\alpha}V\left(t\right) \leqslant -hx^{T}\left(t\right) x\left(t\right) ,\tag{36}$$

then ||x(t)|| and ||y(t)|| are bounded for all t > 0, and x(t) converges to zero asymptotically.

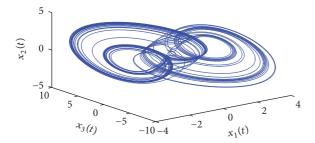


FIGURE 2: Fractional-order Arneodo system.

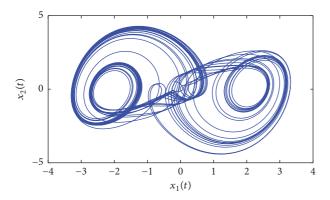


FIGURE 3: The chaotic behavior of fractional-order Arneodo system in x_1 - x_2 plane.

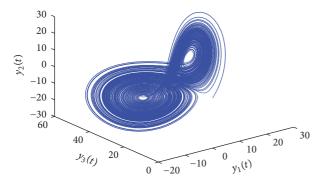


FIGURE 4: Fractional-order Lorenz system.

Proof. From (36), we have

$$D_{t}^{\alpha}V_{2}(t) \leq -hx^{T}(t)x(t) \leq 0.$$
 (37)

Based on Lemma 11, we know that $V_2(t)$ is monotonically decreasing in $[0, +\infty]$. Then

$$V_2(t) \le V_2(0)$$
. (38)

Thus, $\|x(t)\| \le \sqrt{2V_2(0)}$ and $\|y(t)\| \le \sqrt{2V_2(0)}$; namely, $\|x(t)\|$ and $\|y(t)\|$ are bounded. Next we will prove that x(t) tends to 0 asymptotically. Taking α th integral on both sides of (37), we have

$$V_2(t) - V_2(0) \le -hD_t^{-\alpha} x^T(t) x(t).$$
 (39)

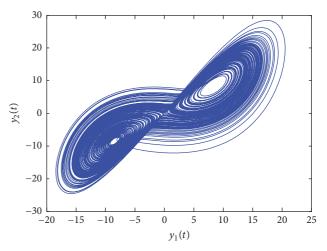


FIGURE 5: The chaotic behavior of fractional-order Lorenz system in y_1 - y_2 plane.

Noting that $V_2(t) = (1/2)x^T(t)x(t) + (1/2)y^T(t)y(t)$, we have $x^T(t)x(t) \le 2V_2(t)$. Consequently,

$$x^{T}(t) x(t) \le 2V_{2}(0) - 2hD_{t}^{-\alpha} x^{T}(t) x(t).$$
 (40)

Thus, we can find a nonnegative function Z(t) such that

$$x^{T}(t) x(t) + Z(t) = 2V_{2}(0) - 2hD_{t}^{-\alpha}x^{T}(t) x(t)$$
. (41)

Taking Laplace transform on both sides of (41), we have

$$X^{T}(s) X(s) = 2V_{2}(0) \frac{s^{\alpha-1}}{s^{\alpha} + 2h} - \frac{s^{\alpha}}{s^{\alpha} + 2h} Z(s).$$
 (42)

According to (30), the solution of (42) is

$$x^{T}(t) x(t) = 2V_{2}(0) E_{\alpha,0}(-2ht^{\alpha}) - Z(t)$$

$$* \left[t^{-1} E_{\alpha,0}(-2ht^{\alpha})\right],$$
(43)

where * is convolution. Because t^{-1} and $E_{\alpha,0}(-2ht^{\alpha})$ are nonnegative functions, it follows from Lemma 12 that x(t) converges to zero asymptotically. This completes the proof of Lemma 13.

Remark 14. If $x^T(t)x(t) \leq 2V_2(0)E_\alpha(-2ht^\alpha)$, we know that x(t) will tend to 0 asymptotically according to the results in [48]. Namely, $\lim_{t\to\infty} ||x(t)|| = 0$.

3.3. Stability Analysis

Theorem 15. If d(t) = 0, we can realize the synchronization of system (12) and (13) under the effect of the adaptive controller (24) and the fractional-order adaptive law (25). And all the variables in the closed-loop system remain bounded.

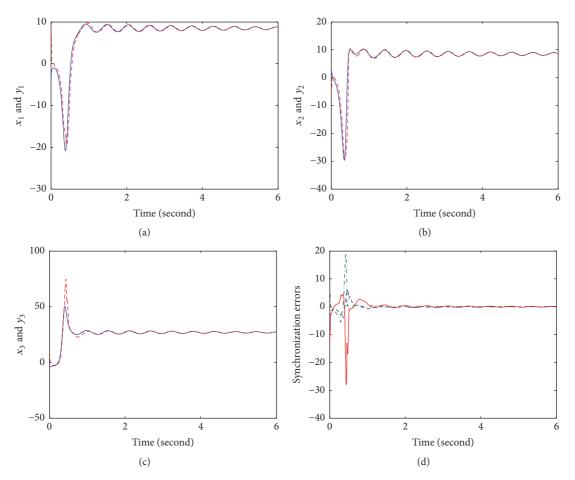


FIGURE 6: Synchronization results: (a) $x_1(t)$ (solid line) and $y_1(t)$ (dashed-dotted line); (b) $x_2(t)$ (solid line) and $y_2(t)$ (dashed-dotted line); and (c) $x_3(t)$ (solid line) and $y_3(t)$ (dashed-dotted line). (d) Synchronization errors: $e_1(t)$ (dashed line), $e_2(t)$ (dashed-dotted line), and $e_3(t)$ (solid line).

Proof. Substituting the synchronization controllers (24) and (23) into the error dynamical equation (19), we have

$$D_{t}^{\alpha}e(t) = Ce(t) + h(t) - Ke(t) - \mathcal{W}^{T}\varphi(x)$$

$$-H \operatorname{sign}(e(t))$$

$$= -(K - C)e(t) + \varepsilon(t) - \widetilde{\mathcal{W}}^{T}\varphi(x) \qquad (44)$$

$$-H \operatorname{sign}(e(t))$$

$$= -Pe(t) + \varepsilon(t) - \widetilde{\mathcal{W}}^{T}\varphi(x) - H \operatorname{sign}(e(t)),$$

where P = K - C. We can choose an appropriate gain matrix K such that P is a positive definite matrix. Multiplying $e^{T}(t)$ on both sides of (44) yields

$$e^{T}(t) D_{t}^{\alpha} e(t) = -e^{T}(t) Pe(t) + e^{T}(t) \epsilon(t)$$
$$-e^{T}(t) \widetilde{\mathcal{W}}^{T} \varphi(x)$$
$$-e^{T}(t) H \operatorname{sign}(e(t))$$

$$\leq -e^{T}(t) \operatorname{Pe}(t) + \sum_{i=1}^{n} |e_{i}(t)| e_{i}^{*}(t)$$

$$- \sum_{i=1}^{n} e_{i}(t) \widetilde{W}_{i}^{T} \varphi_{i}(x)$$

$$- \sum_{i=1}^{n} |e_{i}(t)| e_{i}^{*}(t)$$

$$\leq -e^{T}(t) \operatorname{Pe}(t) - \sum_{i=1}^{n} e_{i}(t) \widetilde{W}_{i}^{T} \varphi_{i}(x).$$

$$(45)$$

Consider the following Lyapunov function:

$$V(t) = \frac{1}{2}e^{T}(t) e(t) + \frac{1}{2} \sum_{i=1}^{n} \frac{1}{\mu_{i}} \widetilde{W}_{i}^{T} \widetilde{W}_{i}.$$
 (46)

Because the α th Caputo derivative of a constant is 0, we have $D_t^{\alpha}\widetilde{W}_i=D_t^{\alpha}W_i$. Taking α th derivative of V(t) based on Lemma 10 gives

$$D_t^{\alpha}V(t) \leq e^T(t)D_t^{\alpha}e(t) + \sum_{i=1}^n \frac{1}{\mu_i}\widetilde{\mathcal{W}}_i^T D_t^{\alpha}\mathcal{W}_i. \tag{47}$$

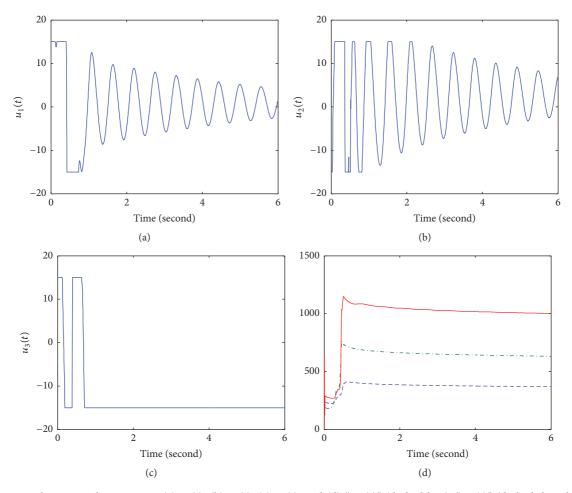


FIGURE 7: Control inputs and parameters: (a) $u_1(t)$; (b) $u_2(t)$; (c) $u_3(t)$; and (d) $||W_1(t)||$ (dashed line), $||W_2(t)||$ (dashed-dotted line), and $||W_3(t)||$ (solid line).

Substituting (45) and (25) into (47), we have

$$D_{t}^{\alpha}V(t) \leq -e^{T}(t) Pe(t) - \sum_{i=1}^{n} e_{i}(t) \widetilde{\mathcal{W}}_{i}^{T} \varphi_{i}(x)$$

$$+ \sum_{i=1}^{n} \frac{1}{\mu_{i}} \widetilde{\mathcal{W}}_{i}^{T} D_{t}^{\alpha} \mathcal{W}_{i}$$

$$\leq -e^{T}(t) Pe(t) - \sum_{i=1}^{n} e_{i}(t) \widetilde{\mathcal{W}}_{i}^{T} \varphi_{i}(x)$$

$$+ \sum_{i=1}^{n} e_{i}(t) \widetilde{\mathcal{W}}_{i}^{T} \varphi_{i}(x) \leq -e^{T}(t) Pe(t)$$

$$\leq -\lambda_{\min} e^{T}(t) e(t),$$

$$(48)$$

where λ_{\min} is the minimum eigenvalue of matrix P. From (48) and Lemma 13, we know that the synchronization error e(t) tends to 0 asymptotically; namely, $\lim_{t\to\infty} \|e(t)\| = 0$.

Theorem 16. We can realize the synchronization of system (12) and (13) under the effect of the adaptive controller (24) and the fractional-order adaptive laws (see (25) and (26)). And

all variables in the closed-loop system remain bounded when $d(t) \neq 0$.

Proof. Substituting (23) and (24) into the error dynamical equation (19), we obtain

$$D_{t}^{\alpha}e(t) = Ce(t) + h(t) + d(t) - Ke(t) - \mathcal{W}^{T}\varphi(x)$$

$$- H \operatorname{sign}(e(t)) - \widehat{\rho} \operatorname{sign}(e(t))$$

$$= -(K - C)e(t) + d(t) + \varepsilon(t) - \widetilde{\mathcal{W}}^{T}\varphi(x)$$

$$- H \operatorname{sign}(e(t)) - \widehat{\rho} \operatorname{sign}(e(t))$$

$$\leq -Pe(t) + \varepsilon(t) - \widetilde{\mathcal{W}}^{T}\varphi(x) - H \operatorname{sign}(e(t))$$

$$- \widetilde{\rho} \operatorname{sign}(e(t)),$$

$$(49)$$

where P = K - C is a positive matrix.

$$\widetilde{\rho}_i(t) = \widehat{\rho}_i(t) - \rho_i. \tag{50}$$

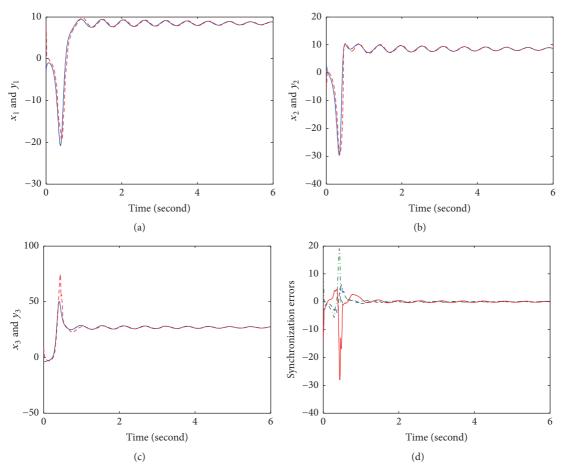


FIGURE 8: Synchronization results: (a) $x_1(t)$ (solid line) and $y_1(t)$ (dashed-dotted line); (b) $x_2(t)$ (solid line) and $y_2(t)$ (dashed-dotted line); and (c) $x_3(t)$ (solid line) and $y_3(t)$ (dashed-dotted line). (d) Synchronization errors: $e_1(t)$ (dashed line), $e_2(t)$ (dashed-dotted line), and $e_3(t)$ (solid line).

Multiplying $e^{T}(t)$ on both sides of (50) gives

$$e^{T}(t) D_{t}^{\alpha} e(t) = -e^{T}(t) Pe(t) + e^{T}(t) \epsilon(t)$$

$$-e^{T}(t) \widetilde{W}^{T} \varphi(x)$$

$$-e^{T}(t) H \operatorname{sign}(e(t))$$

$$-e^{T}(t) \widetilde{\rho} \operatorname{sign}(e(t))$$

$$\leq -e^{T}(t) Pe(t) + \sum_{i=1}^{n} |e_{i}(t)| \epsilon_{i}^{*}(t)$$

$$-\sum_{i=1}^{n} e_{i}(t) \widetilde{W}_{i}^{T} \varphi_{i}(x) - \sum_{i=1}^{n} \epsilon_{i}^{*}(t) |e_{i}(t)|$$

$$-\sum_{i=1}^{n} \widetilde{\rho}_{i}(t) |e_{i}(t)|$$

$$\leq -e^{T}(t) Pe(t) - \sum_{i=1}^{n} e_{i}(t) \widetilde{W}_{i}^{T} \varphi_{i}(x)$$

$$-\sum_{i=1}^{n} \widetilde{\rho}_{i}(t) |e_{i}(t)|.$$
(51)

Consider the following Lyapunov function:

$$V(t) = \frac{1}{2}e^{T}(t)e(t) + \frac{1}{2}\sum_{i=1}^{n}\frac{1}{\mu_{i}}\widetilde{W}_{i}^{T}\widetilde{W}_{i} + \frac{1}{2}\sum_{i=1}^{n}\frac{1}{\gamma_{i}}\widetilde{\rho}_{i}^{2}(t). \quad (52)$$

Taking α th derivative of V(t) based on Lemma 10, we have

$$D_{t}^{\alpha}V(t) \leq e^{T}(t)D_{t}^{\alpha}e(t) + \sum_{i=1}^{n} \frac{1}{\mu_{i}}\widetilde{\mathcal{W}}_{i}^{T}D_{t}^{\alpha}\mathcal{W}_{i}$$

$$+ \sum_{i=1}^{n} \frac{1}{\gamma_{i}}\widetilde{\rho}_{i}(t)D_{t}^{\alpha}\rho_{i}(t).$$
(53)

Substituting (45), (25), and (26) into (53), we have

$$\begin{split} D_{t}^{\alpha}V\left(t\right) &\leqslant -e^{T}\left(t\right)Pe\left(t\right) - \sum_{i=1}^{n}e_{i}\left(t\right)\widetilde{\mathcal{W}}_{i}^{T}\varphi_{i}\left(x\right) \\ &- \sum_{i=1}^{n}\widetilde{\rho}_{i}\left(t\right)\left|e_{i}\left(t\right)\right| + \sum_{i=1}^{n}\frac{1}{\mu_{i}}\widetilde{\mathcal{W}}_{i}^{T}D_{t}^{\alpha}\mathcal{W}_{i} \\ &+ \sum_{i=1}^{n}\frac{1}{\gamma_{i}}\widetilde{\rho}_{i}\left(t\right)D_{t}^{\alpha}\rho_{i}\left(t\right) \end{split}$$

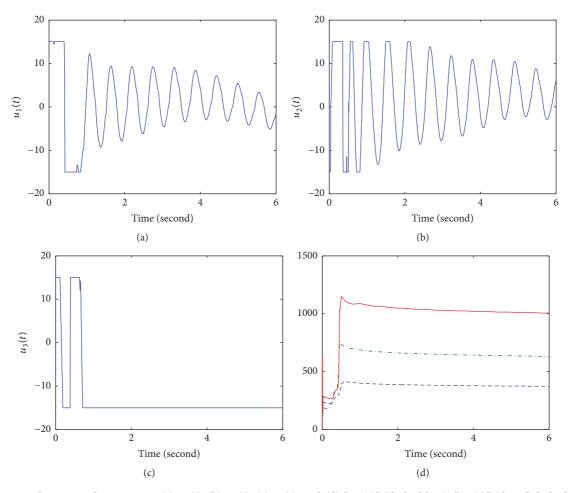


FIGURE 9: Control inputs and parameters: (a) $u_1(t)$; (b) $u_2(t)$; (c) $u_3(t)$; and (d) $||W_1(t)||$ (dashed line), $||W_2(t)||$ (dotted dashed line), and $||W_3(t)||$ (solid line).

$$\leq -e^{T}(t) \operatorname{Pe}(t) - \sum_{i=1}^{n} e_{i}(t) \widetilde{W}_{i}^{T} \varphi_{i}(x)$$

$$- \sum_{i=1}^{n} \widetilde{\rho}_{i}(t) \left| e_{i}(t) \right| + \sum_{i=1}^{n} e_{i}(t) \widetilde{W}_{i}^{T} \varphi_{i}(x)$$

$$+ \sum_{i=1}^{n} \widetilde{\rho}_{i}(t) \left| e_{i}(t) \right| \leq -e^{T}(t) \operatorname{Pe}(t)$$

$$\leq -\lambda_{\min} e^{T}(t) e(t), \tag{54}$$

where λ_{\min} is the minimum eigenvalue of matrix *P*. From (54) and Lemma 13, we know that the synchronization error e(t) tends to 0 asymptotically; namely, $\lim_{t\to\infty} ||e(t)|| = 0$.

4. Simulation Studies

In this section, two fractional-order chaotic systems and two fractional-order hyperchaotic systems will be synchronized to show the validity of the above method.

4.1. Example 1. Choose the frequently used fractional-order Arneodo system [49] in literature as the drive system:

$$D_{t}^{\alpha}x_{1}(t) = x_{2}(t)$$

$$D_{t}^{\alpha}x_{2}(t) = x_{3}(t)$$

$$D_{t}^{\alpha}x_{3}(t) = ax_{1}(t) - bx_{2}(t) - cx_{3}(t) + dx_{1}^{3}(t).$$
(55)

When a = -5.5, b = 3.5, c = 0.4, d = -1, and $\alpha = 0.9$, the fractional-order Arneodo system shows chaotic phenomenon, which is indicated in Figures 2 and 3.

Let the response system be the following fractional-order Lorenz system [50]:

$$D_{t}^{\alpha} y_{1}(t) = \sigma \left(y_{2}(t) - y_{1}(t) \right)$$

$$D_{t}^{\alpha} y_{2}(t) = y_{1}(t) \left(\rho - y_{3}(t) \right) - y_{2}(t)$$

$$D_{t}^{\alpha} y_{3}(t) = y_{1}(t) y_{2}(t) - \beta y_{3}(t).$$
(56)

When $\sigma = 10$, $\rho = 28$, $\beta = 8/3$, and $\alpha = 0.99$, the chaotic behavior of system (56) is included in Figures 4 and 5.

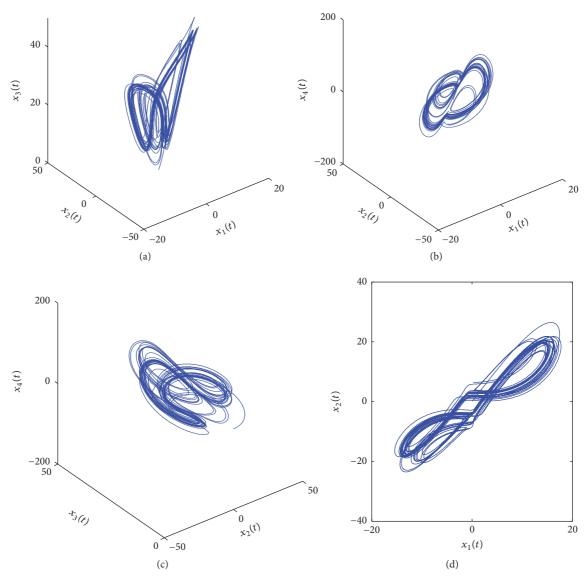


FIGURE 10: Fractional-order hyperchaotic Lorenz system (58).

It follows from (55) and (56) that

$$A = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ a & -b & -c \end{pmatrix}$$

$$C = \begin{pmatrix} -\sigma & \sigma & 0 \\ \rho & -1 & 0 \\ 0 & 0 & -\beta \end{pmatrix}.$$
(57)

Firstly, we consider the synchronization of system (55) and system (56) in the absence of external disturbance (namely, d(t) = 0). In the simulation, we choose $\sigma = 0.8$, $\alpha = 0.96$, and $k_1 = k_2 = k_3 = 3$. The initial condition of system (55) is $x(0) = [-3, 3.4, -4]^T$, and the initial condition

of system (56) is $y(0) = [8, -6, 9]^T$. With respect to the fuzzy logic system, we define 6 Gaussian membership functions uniformly distributed on $[-20\ 20]$. The initial condition of the fuzzy parameter is chosen as zero vector. The input saturation limiter $u_r = -u_l = 5$. The simulation results are depicted in Figures 6 and 7.

Then we study the synchronization of system (55) and system (56) with the external disturbance. In simulation, we select $\sigma = 0.8$, $\alpha = 0.96$, and $k_1 = k_2 = k_3 = 3$. The initial conditions are $x(0) = [-3, 3.4, -4]^T$ and $y(0) = [8, -6, 9]^T$. Let $d(t) = [0.15\sin(t), 0.05\cos(t), 0.1\cos(t)]^T$ and let the input saturation limiter be $u_r = -u_l = 5$. The simulation results are as shown in Figures 8 and 9.

4.2. Example 2. Choose the fractional-order hyperchaotic Lorenz system [50] as the drive system:

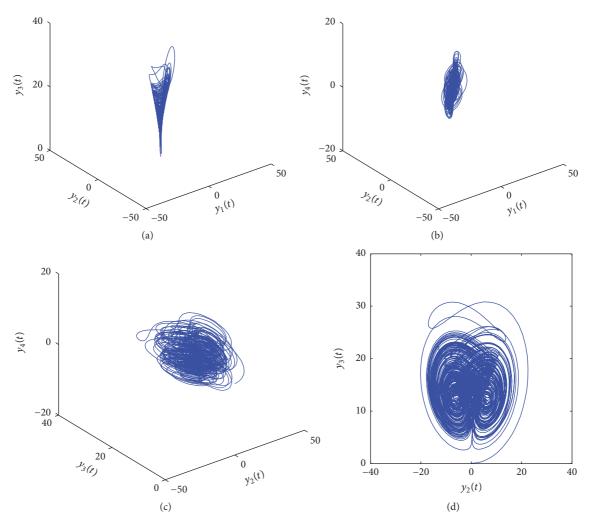


FIGURE 11: Fractional-order hyperchaotic system (59).

$$D_{t}^{\alpha}x_{1}(t) = a(x_{2}(t) - x_{1}(t)) + x_{4}(t)$$

$$D_{t}^{\alpha}x_{2}(t) = cx_{1}(t) - x_{2}(t) - x_{1}(t)x_{3}(t)$$

$$D_{t}^{\alpha}x_{3}(t) = x_{1}(t)x_{2}(t) - bx_{3}(t)$$

$$D_{t}^{\alpha}x_{4}(t) = -x_{1}(t)x_{3}(t) + yx_{4}(t).$$
(58)

When a=10, b=8/3, c=28, $\gamma=-1$, and $\alpha=0.93$, the fractional-order hyperchaotic Lorenz system (58) has chaotic

The response system is the following fractional-order hyperchaotic system:

attractors, as shown in Figure 10.

$$D_{t}^{\alpha}y_{1}(t) = a(y_{2}(t) - y_{1}(t))$$

$$D_{t}^{\alpha}y_{2}(t) = dy_{1}(t) - y_{1}(t)y_{3}(t) + cy_{2}(t) - y_{4}(t)$$

$$D_{t}^{\alpha}y_{3}(t) = y_{1}(t)y_{2}(t) - by_{3}(t)$$

$$D_{t}^{\alpha}y_{4}(t) = y_{1}(t) + k.$$
(59)

When a = 36.01, b = 3.00, c = 28.00, d = -16.00, k = 0.50, and $\alpha = 0.95$, the chaotic behavior of system (59) is given in Figure 11.

Firstly, we consider the synchronization of system (58) and system (59) when d(t) = 0. In the simulation, we choose the control parameters as $\sigma = 0.8$, $\alpha = 0.95$, and $k_1 = k_2 = k_3 = k_4 = 3$. The initial conditions are $x(0) = [-6, 2.4, -4, -6]^T$ and $y(0) = [9.6, -6, 9, 5]^T$. The input saturation limiter $u_{r1} = -u_{l1} = 12$ and $u_{ri} = -u_{li} = 14$, i = 2, 3, 4. The simulation results are presented in Figures 12–15.

Then, we consider the synchronization of system (58) and system (59) with external disturbance. In the simulation, let $\sigma=0.8$, $\alpha=0.95$, $k_1=k_2=k_3=k_4=3$, and $d(t)=[0.15\sin(t),0.05\cos(t),0.1\cos(t),0.5\sin(t)\cos(t)]^T$. The initial conditions are $x(0)=[-3,3.4,-4,-6]^T$ and $y(0)=[9.6,-6,9,5]^T$. The input saturation limiter is $u_{r1}=-u_{l1}=12$ and $u_{ri}=-u_{li}=14$, i=2,3,4. The simulation results are depicted in Figures 16–19.

5. Conclusions

In this paper, we investigate the synchronization for two uncertain fractional-order nonlinear chaotic systems with saturated input and external disturbances in accordance with

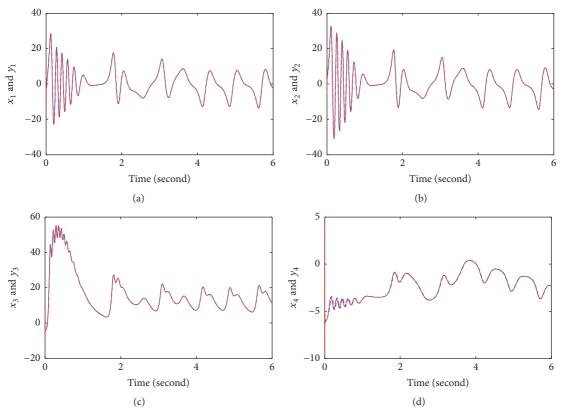


FIGURE 12: Synchronization results: (a) $x_1(t)$ (solid line) and $y_1(t)$ (dashed line); (b) $x_2(t)$ (solid line) and $y_2(t)$ (dashed line); (c) $x_3(t)$ (solid line) and $y_3(t)$ (dashed line); and (d) $x_4(t)$ (solid line) and $y_4(t)$ (dashed line).

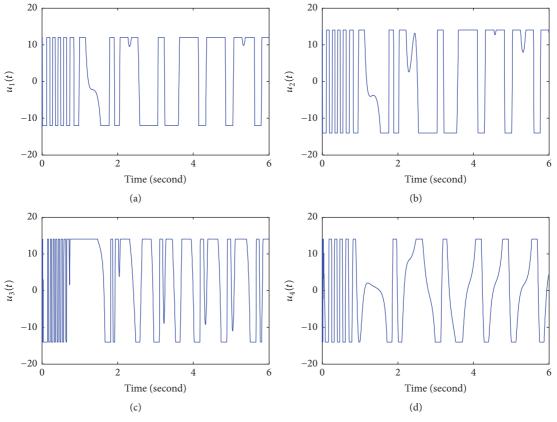


Figure 13: Control inputs: (a) $u_1(t)$; (b) $u_2(t)$; (c) $u_3(t)$; and (d) $u_4(t)$.

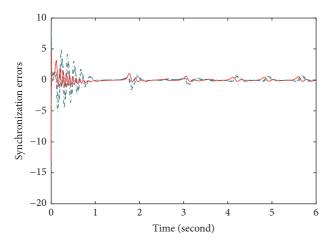


FIGURE 14: Synchronization errors: $e_1(t)$ (dotted line), $e_2(t)$ (dotted dashed line), $e_3(t)$ (solid line), and $e_4(t)$ (dashed line).

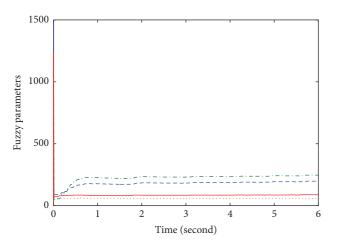


FIGURE 15: Parameters: $||W_1(t)||$ (dotted line), $||W_2(t)||$ (dotted dashed line), $||W_3(t)||$ (solid line), and $|W_4(t)|$ (dashed line).

the fractional Lyapunov stability theory and adaptive fuzzy control method. A fractional-order adaptive controller that can guarantee that the synchronization error tends to a small region of origin and fractional parameters adaptive laws are designed. Based on the proposed method, we can achieve synchronization of many fractional-order chaotic systems and hyperchaotic systems. It should be mentioned that the proposed controller can guarantee that the synchronization errors converge to a small region of the origin eventually. How to design an adaptive fuzzy controller such that the dynamical system is asymptotic stable is one of our future research directions.

Conflicts of Interest

The authors declare that there are no conflicts of interest regarding the publication of this paper.

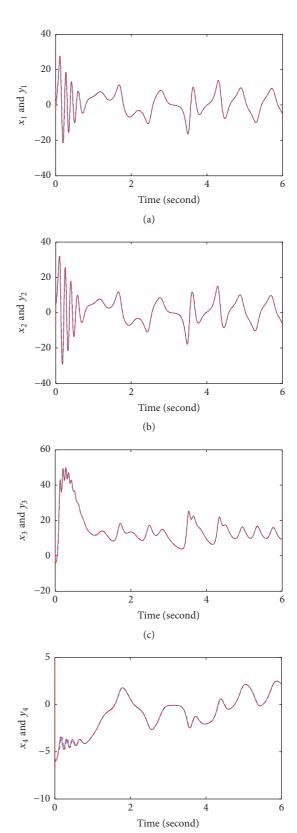


FIGURE 16: Synchronization results: (a) $x_1(t)$ (solid line) and $y_1(t)$ (dashed line); (b) $x_2(t)$ (solid line) and $y_2(t)$ (dashed line); (c) $x_3(t)$ (solid line) and $y_3(t)$ (dashed line); and (d) $x_4(t)$ (solid line) and $y_4(t)$ (dashed line).

(d)

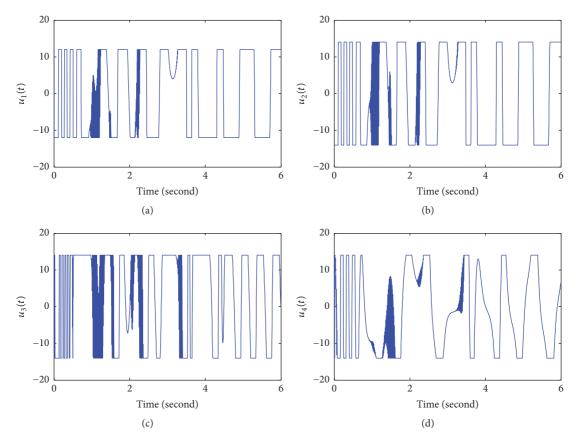


FIGURE 17: Control inputs: (a) $u_1(t)$; (b) $u_2(t)$; (c) $u_3(t)$; and (d) $u_4(t)$.

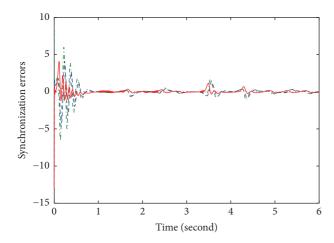


FIGURE 18: Synchronization errors: $e_1(t)$ (dotted line), $e_2(t)$ (dot dash line), $e_3(t)$ (solid line), and $e_4(t)$ (dashed line).

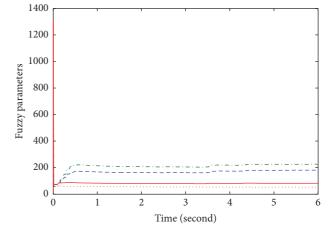


FIGURE 19: Parameters: $\|W_1(t)\|$ (dotted line), $\|W_2(t)\|$ (dotted dashed line), $\|W_3(t)\|$ (solid line), and $\|W_4(t)\|$ (dashed line).

Acknowledgments

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